

## Results from GRAPE model (phase 1)

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The integrated assessment model GRAPE (Global Relationship to Protect the Environment) consists of five modules dealing with issues on energy, climate, land use, macroeconomics and environmental impacts. The results for the assessment of contributions to climate change (phase 1) are summarized as follows.

### [1] Assessment framework and input data

Emissions or radiative forcing data, shown in the table below, are given to obtain global average surface atmospheric temperature change. IPCC WGI TAR A2 scenario data and own assumptions are used to supplement information specified by the project.

Table.1 Input Data

|                          | Emissions |        | Concentration |         | Radiative Forcing |
|--------------------------|-----------|--------|---------------|---------|-------------------|
|                          | Past      | Future | Pre-ind.      | Current | Future            |
| CO2                      |           |        | (*2)          | (*2)    | Endogenous        |
| Fossil Fuel              | (*1)      | (*1)   |               |         |                   |
| LULUCF                   | (*1)      | (*1)   |               |         |                   |
| CH4                      | (*3)      | (*1)   | (*2)          | (*2)    | Endogenous        |
| N2O                      | (*3)      | (*1)   | (*2)          | (*2)    | Endogenous        |
| Other GHGs (#)           |           |        |               |         | (*2)              |
| Aerosol                  |           |        |               |         | (*2)              |
| SOx ( direct, indirect ) |           |        |               |         | (*2)              |
| others ( BC,OC )         |           |        |               |         | (*2)              |

(#) PFC,SF6,HFC,Montreal Gases(CFC,etc.) ,Ozone, etc.

(\*1) Data specified by the project

(\*2) IPCC WGI TAR

(\*3) Own assumptions

### [2] Reporting parameters

#### (1)Historical anthropogenic emissions

Historical emissions after industrial revolution period is important data to verify present GHGs concentration level and climate model benchmarks. The assumption of anthropogenic emissions of CO2, CH4 and N2O after 1760 is summarized in Table 2. CO2 and CH4 data are from CDIAC (ORNL). N2O emissions are obtained by own assumption climate model in the Appendix.

Table 2 Historical anthropogenic emissions

|                | 1760 | 1770 | 1780 | 1790 | 1800 | 1810 | 1820 | 1830 | 1840 | 1850 | 1860 | 1870 | 1880 | 1890 | 1900 | 1910 | 1920 | 1930 | 1940 | 1950 | 1960 | 1970 | 1980 | 1990 |
|----------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| CO2 (GtonC)    | 0.22 | 0.24 | 0.26 | 0.29 | 0.31 | 0.32 | 0.33 | 0.35 | 0.37 | 0.40 | 0.45 | 0.51 | 0.65 | 0.85 | 1.02 | 1.38 | 1.27 | 1.36 | 1.51 | 1.88 | 3.12 | 4.84 | 5.99 | 7.10 |
| CH4 (Mton-CH4) | 25   | 30   | 35   | 40   | 45   | 50   | 55   | 60   | 65   | 70   | 79   | 85   | 92   | 103  | 114  | 130  | 137  | 149  | 162  | 178  | 221  | 276  | 319  | 310  |
| N2O (Mton-N)   | 2.00 | 2.00 | 2.00 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 | 2.20 | 2.30 | 2.40 | 2.50 | 2.60 | 2.80 | 3.00 | 3.30 | 3.80 | 5.00 | 6.7  |

(2) Cumulative emissions after 1990

Cumulative Emissions after 1990 are shown in Table 3. Since IPCC SRES A2 is specified as future GHG emission data, marker results from ASF model are used. Assumed cumulative emission up to 2100 for CO2, CH4 and N2O are 276Gton-C, 8590Mton-CH4 and 161Mton-N, respectively.

Table 3 Cumulative emissions after 1990

| Cumulative Emissions after 1990 | 2000 | 2010 | 2020  | 2030  | 2040  | 2050  | 2060  | 2070  | 2080  | 2090  | 2100  |
|---------------------------------|------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| CO2 (GtonC)                     | 75   | 163  | 272   | 407   | 561   | 729   | 912   | 1112  | 1332  | 1579  | 1855  |
| CH4 (Mton-CH4)                  | 3163 | 6629 | 10602 | 15152 | 20288 | 25983 | 32243 | 39073 | 46479 | 54473 | 63064 |
| N2O (Mton-N)                    | 68   | 144  | 232   | 333   | 443   | 559   | 684   | 818   | 962   | 1114  | 1275  |

(3) Atmospheric GHG concentrations

The gas in the atmosphere is balanced with emissions (sum of anthropogenic and natural) and gas decay. Historical atmospheric concentration of CO2, CH4 and N2O are approximately consistent with IPCC WGI TAR. Atmospheric concentration of CO2, CH4 and N2O in 2100 are calculated 971(ppm), 3325(ppb) and 449(ppb), respectively.

Table 4 Atmospheric concentration

|           | 1760 | 1770 | 1780 | 1790 | 1800 | 1810 | 1820 | 1830 | 1840 | 1850 | 1860 | 1870 | 1880 | 1890 | 1900 | 1910 | 1920 | 1930 | 1940 | 1950 | 1960 | 1970 | 1980 |
|-----------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| CO2 (ppm) | 282  | 282  | 282  | 283  | 283  | 284  | 284  | 285  | 285  | 286  | 286  | 287  | 288  | 290  | 292  | 295  | 298  | 300  | 303  | 306  | 313  | 324  | 339  |
| CH4 (ppb) | 707  | 718  | 732  | 746  | 760  | 774  | 788  | 803  | 817  | 832  | 850  | 869  | 888  | 912  | 942  | 983  | 1027 | 1072 | 1125 | 1190 | 1274 | 1403 | 1551 |
| N2O (ppb) | 271  | 273  | 274  | 275  | 276  | 278  | 279  | 280  | 281  | 281  | 282  | 283  | 284  | 284  | 285  | 286  | 287  | 288  | 290  | 291  | 293  | 296  | 300  |

|           | 1990 | 2000 | 2010 | 2020 | 2030 | 2040 | 2050 | 2060 | 2070 | 2080 | 2090 | 2100 |
|-----------|------|------|------|------|------|------|------|------|------|------|------|------|
| CO2 (ppm) | 352  | 367  | 419  | 461  | 511  | 565  | 622  | 681  | 744  | 812  | 887  | 971  |
| CH4 (ppb) | 1700 | 1760 | 1839 | 1962 | 2116 | 2283 | 2453 | 2623 | 2795 | 2969 | 3146 | 3325 |
| N2O (ppb) | 308  | 316  | 325  | 335  | 348  | 361  | 374  | 388  | 402  | 417  | 433  | 449  |

(4) Radiative forcing

Radiative forcing of CO2, CH4 and N2O is endogenously assessed by the atmospheric

concentration above. On the other hand, radiative forcing by Kyoto Protocol gases such as PFCs, HFCs and SF6, Montreal Protocol gases, Ozone, sulfate and other aerosol are followed by IPCC WGI TAR A2 scenario. Radiative forcing relative to pre-industrial level is as follows.

Table 5 Radiative forcing relative to pre-industrial level

| Radiative Forcing   | 2000 | 2010 | 2020 | 2030 | 2040 | 2050 | 2060 | 2070 | 2080 | 2090 | 2100 |
|---------------------|------|------|------|------|------|------|------|------|------|------|------|
| (W/m <sup>2</sup> ) | 2.19 | 2.92 | 3.77 | 4.45 | 5.14 | 5.85 | 6.50 | 7.15 | 7.80 | 8.49 | 9.19 |

(5) Temperature rise (global mean surface air temperature)

Simple atmosphere-ocean model in the Appendix provides global mean atmospheric temperature in the Table 6. Temperature rise in 2100 relative to 1990 is approximately 4 deg C.

Table 6 Global mean surface air temperature rise relative to 1990

|       | 2000 | 2010 | 2020 | 2030 | 2040 | 2050 | 2060 | 2070 | 2080 | 2090 | 2100 |
|-------|------|------|------|------|------|------|------|------|------|------|------|
| deg C | 0.16 | 0.55 | 0.97 | 1.37 | 1.76 | 2.15 | 2.53 | 2.90 | 3.27 | 3.65 | 4.03 |

[3] Works for Phase 2

We have noticed that the results above are relatively high in terms of CO<sub>2</sub> concentration, radiative forcing and temperature rise, compared to the IPCC TAR WGI reference run by ISAM and BERN model. In phase 2, we are planning to estimate future CO<sub>2</sub> concentration assessment using simple BERN model prepared by the project web site for the assessment of contributions to climate change, which will provide different concentration, radiative forcing and temperature level. Sea level rise by thermal expansion will be assessed also.

## Appendix: Model Structure

Climate module structure of GRAPE depends on the previous modeling framework such as Mori [1], IPCC WGI TAR [3] and RITE/NEDO [3].

### (1) Emission - concentration

Emission - concentration relationship of CO<sub>2</sub>, CH<sub>4</sub> and N<sub>2</sub>O are summarized as follows.

#### a. CO<sub>2</sub> [1]

Atmospheric concentration of CO<sub>2</sub> is given by the sum of the ones from previous periods with different time constants and emissions remaining in the atmosphere.

$$C_{CO_2,t} = \sum_{i=1}^5 C\_TLAG_{i,t} \quad (1)$$

$$C\_TLAG_{i,t+1} = C\_TLAG_{i,t} \cdot e^{-BSHR_i \cdot \Delta T} + \int_0^{\Delta T} ASHR_i \cdot E_{CO_2} dt \quad (2)$$

where  $C_{CO_2,t}$  atmospheric CO<sub>2</sub> at t (GtonC),  
 $C\_TLAG_{i,t}$  atmospheric CO<sub>2</sub> at t with ith time constant (GtonC)  
 $BSHR_i$  decay parameter  
 $ASHR_i$  distribution fraction of ith composition(---)  
 $E_{CO_2,t}$  CO<sub>2</sub> Emission at time t (GtonC)  
 $\Delta T$  time step

Future CO<sub>2</sub> concentration can be assumed by the initial concentration composition. Time step  $\Delta T=10$ (years) in the simulation. Parameter ASHR and BSHR are from Enting et.al. [4]

|     | ASHR     | BSHR(1/yr) | C_TLAG <sub>1990</sub> |
|-----|----------|------------|------------------------|
| i=1 | 0.130164 | 0.0        | 642.9                  |
| i=2 | 0.333279 | 0.024127   | 11.245                 |
| i=3 | 0.260540 | 0.0116449  | 28.689                 |
| i=4 | 0.165742 | 0.0017107  | 34.3652                |
| i=5 | 0.110275 | 0.00024156 | 36.8351                |

Historical CO<sub>2</sub> concentration is estimated by BERN model parameter specified in the project web page. BSHR is the reciprocal number of time constant of ith fraction.

|     | ASHR  | BSHR(1/yr) |
|-----|-------|------------|
| i=1 | 0.152 | 0.0        |
| i=2 | 0.253 | 0.0058480  |
| i=3 | 0.279 | 0.0555556  |
| i=4 | 0.316 | 0.3891051  |

Differential equation of (2) is given by the following.

$$C\_TLAG_{i,t} = C\_TLAG_{i,t-1} \cdot e^{-BSHR_i} + ASHR_i \cdot \Delta T \cdot \frac{E_{CO2,t} + E_{CO2,t}}{2} \quad (3)$$

The concentration is obtained by applying the conversion factor 0.471(ppm/GtonC) after each period atmospheric CO2 concentration from (3).

b. CH4 and N2O [2]

It is assumed that CH4 and N2O behaviors follow the one-box model in the equation (4).

$$\frac{dC_i}{dt} = \alpha_i E_i - \frac{C_i}{\tau_i} \quad (4)$$

$$i = CH_4, N_2O$$

where C:concentration(ppb), E:emission ( Mton-CH4 or Mton-N )  
 $\alpha$ :emission - concentration conversion factor,  
 $\tau$ :time constant of decay (years)

In the simulation, time constant of CH4 and N2O are from IPCC WGI TAR (e.g.  $\tau_{CH4}=12.0$ (years),  $\tau_{N2O}=114.0$ (years)). Differential equation from 1990 and 2000 data provides for 10-year time step. They are  $\alpha_{CH4}=0.253$ (ppb/Mton-CH4),  $\alpha_{N2O}=0.210$ (ppb/Mton-N2O).

Differential form of (4) is given by the following (index i is omitted).

$$\frac{C_{t+1} - C_t}{\Delta T} = \alpha \frac{E_{t+1} + E_t}{2} - \frac{1}{\tau} \frac{C_{t+1} + C_t}{2} \quad (5)$$

(2)Concentration – radiative forcing [2]

Concentration – radiative forcing formula follows by the simplified expressions in IPCC WGI TAR.

$$\begin{aligned} \Delta F_{CO2} &= \beta_{CO2} \cdot \ln(C_{CO2} / C_{CO2,0}) \\ \Delta F_{CH4} &= \beta_{CH4} \cdot (\sqrt{C_{CH4}} - \sqrt{C_{CH4,0}}) - (f(C_{CH4}, C_{N2O,0}) - f(C_{CH4,0}, C_{N2O,0})) \\ \Delta F_{N2O} &= \beta_{N2O} \cdot (\sqrt{C_{CH4}} - \sqrt{C_{CH4,0}}) - (f(C_{CH4}, C_{N2O,0}) - f(C_{CH4,0}, C_{N2O,0})) \end{aligned} \quad (6)$$

where  $\Delta F$  : radiative forcing increase relative to pre-industrial level ( W/m2 )

$\beta$ : conversion factor to the radiative forcing

$$f(X, Y) = 0.47 \ln \left[ 1 + 2.01 \times 10^{-5} (XY)^{0.75} + 5.31 \times 10^{-15} X (XY)^{1.52} \right]$$

0 is the subscript representing pre-industrial period.

Parameter  $\beta$  and concentrations in the pre-industrial level is as follows.

|     | $\beta$ | $C_o$    |
|-----|---------|----------|
| CO2 | 5.35    | 278(ppm) |

CH4 0.036 700(ppb)  
 N2O 0.12 270(ppb)

(3) Radiative forcing - temperature [1]

Temperature behavior is modeled by the energy exchange between ocean and atmosphere in the global scale. The formulas of temperature change are given by the following.

$$\frac{dT_E}{dt} = C_1(\Delta F - \lambda T_E - C_2(T_E - T_L)) \quad (7)$$

$$\frac{dT_L}{dt} = C_3(T_E - T_L) \quad (8)$$

where  $T_E$ : atmospheric temperature rise relative to the pre-industrial level(degC)  
 $T_L$ : lower ocean temperature rise relative to the pre-industrial level(degC)  
 $\lambda$ : climate feedback factor  
 $\Delta F$ : increase of radiative forcing relative to the pre-industrial level ( W/m2 )  
 $C_1$ : conversion factor  
 $C_2$ : atmosphere-upper ocean heat transfer coefficient  
 $C_3$ : lower ocean-upper ocean heat transfer coefficient

The parameters in the 10-year step simulation are  $\lambda=1.41, C_1=0.226, C_2=0.440$  and  $C_3=0.02$  respectively.

Reference

[1] S.Mori, "Effects of Carbon Emission Mitigation Options Under Carbon Concentration Stabilization Scenarios", Environment and Economics Policy Studies, Vol.3, No.2, PP.125/142, 2000  
 [2] Climate Change 2001 The Scientific Basis, IPCC, 2001  
 [3] Report of New Earth Program, RITE/NEDO, NEDO-GET-9907, March 2000 (in Japanese)  
 [4] Enting, et.al., Future Emissions and Concentrations of Carbon Dioxide: Key Ocean/ Atmosphere/ Land Analyses, CSIRO Division of Atmospheric Research Technical Paper no. 31, 1994